

Fick's Second Law

CHEN 6603

Fick's 2nd Law

Assume no reaction

Mass Form

$$\frac{\partial(\rho)}{\partial t} = -\nabla \cdot (\mathbf{n}) = -\nabla \cdot \mathbf{v}(\rho) - \nabla \cdot (\mathbf{j})$$

Assume ρ_t is constant

$$\frac{\partial(\omega)}{\partial t} = -\nabla \cdot \mathbf{v}(\omega) - \frac{1}{\rho_t} \nabla \cdot (\mathbf{j})$$

$$(\mathbf{j}) = -\rho_t [D^o](\nabla \omega)$$

$$\frac{\partial(\omega)}{\partial t} + \nabla \cdot \mathbf{v}(\omega) = \nabla \cdot [D^o](\nabla \omega)$$

Assume $[D^o]$ is constant

$$\frac{\partial(\omega)}{\partial t} + \nabla \cdot \mathbf{v}(\omega) = [D^o](\nabla^2 \omega)$$

Molar Form

$$\frac{\partial(c)}{\partial t} = -\nabla \cdot (\mathbf{N}) = -\nabla \cdot \mathbf{u}(c) - \nabla \cdot (\mathbf{J})$$

Assume c_t is constant

$$\frac{\partial(x)}{\partial t} = -\nabla \cdot \mathbf{u}(x) - \frac{1}{c_t} \nabla \cdot (\mathbf{J})$$

$$(\mathbf{J}) = -c_t [D](\nabla x)$$

$$\frac{\partial(x)}{\partial t} + \nabla \cdot \mathbf{u}(x) = \nabla \cdot [D](\nabla x)$$

Assume $[D]$ is constant

$$\frac{\partial(x)}{\partial t} + \nabla \cdot \mathbf{u}(x) = [D](\nabla^2 x)$$

Fick's Law
(simplified)

- Does this describe multicomponent effects?
- When is it reasonable to assume that $[D]$ is constant?

Scaling & Fick's Second Law

$$\frac{\partial(x)}{\partial t} + \nabla \cdot \mathbf{u}(x) = [D](\nabla^2 x)$$

Non-dimensionalization: we have length scale, time scale, and D .

$$t^* = \frac{t}{\tau} \quad \text{Dimensionless time}$$

$$\mathbf{x}^* = \frac{\mathbf{x}}{\ell} \quad \text{Dimensionless space}$$

$$D^* = D \frac{\tau}{\ell^2} \quad \text{Dimensionless diffusivity}$$

$$\text{If } D^*=1 \text{ then } \tau = \frac{\ell^2}{D}$$

- Given D , we can estimate how long it will require for a species to diffuse distance ℓ .
- Given D , we can estimate how far the diffusion boundary layer will reach in time τ .
- If we measure the time that it takes to detect a species that diffuses some distance ℓ through a pure fluid, we can estimate the binary diffusion coefficient for that species in that fluid at the given temperature and pressure.

Diffusion Equations

“Generic” simplified form: $\frac{\partial \phi}{\partial t} + \nabla \cdot \mathbf{v} \phi = D_{\phi} \nabla^2 \phi$

Temperature (Fourier’s Law of Conduction)

- constant properties
- No heat released by chemical reactions
- low Mach numbers (negligible viscous heating)
- No species diffusion
- Pressure is steady.

For systems
with flow

$$\frac{\partial T}{\partial t} + \nabla \cdot \mathbf{v} T = \frac{k}{\rho c_p} \nabla^2 T$$
$$\frac{\partial T}{\partial t} = \frac{k}{\rho c_p} \nabla^2 T$$

Velocity (Newton’s Law of Viscosity)

- constant properties
- pressure & density are constant
- no body forces

$$\frac{\partial \mathbf{v}}{\partial t} + \nabla \cdot (\mathbf{v} \mathbf{v}) = \frac{\mu}{\rho} \nabla^2 \mathbf{v}$$

Note: the form without the convective term is meaningless in the case of momentum.

Species (Fick’s 2nd Law)

- Constant properties
- Pressure is constant
- Body forces act equally
- No reaction.
- No thermal diffusion (Soret effect)

$$\frac{\partial(x)}{\partial t} + \nabla \cdot \mathbf{u}(x) = [D](\nabla^2 x)$$
$$\frac{\partial(x)}{\partial t} = [D](\nabla^2 x)$$

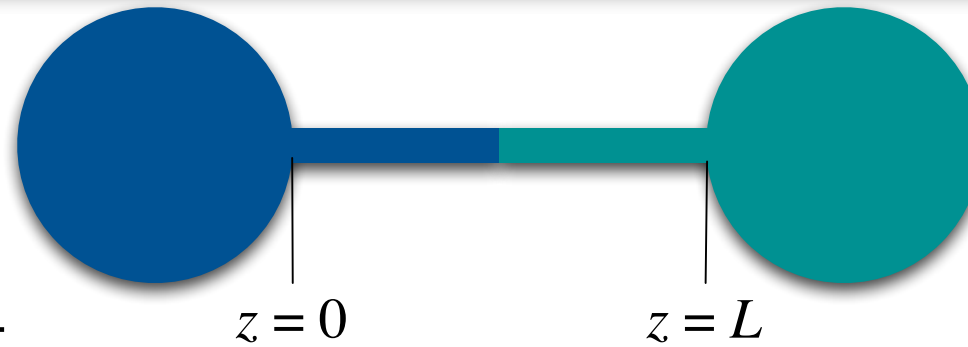


Example: 2 Bulb Problem

(Equimolar Counterdiffusion)

Assume:

- T, p are constant
- No reaction
- 1-D domain $z=[0,L]$
- Compositions are constant at domain boundaries $z=0, z=L$.
- Ideal gas behavior.



$$\begin{aligned} x_i &= x_{i0} & z=0, \\ x_i &= x_{iL} & z=L, \end{aligned}$$

Molar reference frame is most convenient, because $u_z = \text{constant}$ for an ideal gas mixture in 1D. (we can also deduce that $u_z = 0$)

$$\frac{\partial c_t}{\partial t} = -\nabla \cdot c_t \mathbf{u} + \sum_{i=1}^n \frac{s_i}{M_i} \quad c_t = \bar{V}^{-1} = \frac{P}{RT}$$

At “steady state,” $[D](\nabla^2 x) = 0,$

Equations are decoupled because diffusive fluxes are constant.

$$\begin{aligned} \frac{d^2(x)}{dz^2} &= 0, \\ \frac{d(x)}{dz} &= (C_1), \\ (x) &= (C_1)z + (C_2), \end{aligned}$$

get C_1, C_2 using the BCs,

$$(x) = \frac{(x_L) - (x_0)}{L} z + (x_0)$$

Diffusive fluxes can be calculated using:

$$\begin{aligned} (J) &= -c_t [D] \left(\frac{\partial x}{\partial z} \right), \\ &= -\frac{c_t}{L} [D] (x_L - x_0). \end{aligned}$$

Example - Balance on “Bulbs”

Assume:

- T, p are constant
- No reaction
- 1-D domain $z=[0, L]$
- Each bulb is well-mixed (no spatial gradients)
- Ideal gas behavior

 $z = 0$ $z = L$

$$x_i = x_{i0} \quad z = 0,$$

$$x_i = x_{iL} \quad z = L,$$

- @ $t=0$, each bulb has a known composition.
- @ $t=\infty$, we can determine the composition (equilibrium).
- Can we determine the composition in each bulb as a function of time?

Mole balance on a bulb:

$$c_t \frac{\partial x_i}{\partial t} = -\nabla \cdot \mathbf{N}_i$$

$$\int_V c_t \frac{\partial x_i}{\partial t} dV = - \int_S \mathbf{N}_i \cdot \mathbf{a} dS$$

$$c_t V \frac{\partial x_i}{\partial t} = -\mathbf{N}_i A = -\mathbf{J}_i A \quad (\text{because } \mathbf{u} = 0).$$

What assumptions
have been made?

Need to get \mathbf{J}_i ...

For the bulb at $z=0$:

$$c_t V_0 \frac{dx_i^0}{dt} = -\mathbf{J}_i A$$

$$V_0 \frac{dx_i^0}{dt} = A \sum_{j=1}^{n-1} D_{ij} \frac{x_j^L - x_j^0}{L}$$

$$\frac{d(x^0)}{dt} = \frac{A}{LV_0} [D] ((x^L) - (x^0))$$

Recall from our previous discussion
(Fick's second law):

$$(x) = \frac{(x^L) - (x^0)}{L} z + (x^0)$$

$$(J) = -\frac{c_t}{L} [D] (x^L - x^0).$$

What were the assumptions?

Use equilibrium balance to eliminate (x^L) :
(assume tube has “negligible” volume)

$$\begin{aligned} V_0 x_i^0 + V_L x_i^L &= (V_0 + V_L) x_i^\infty, \\ x_i^L &= x_i^\infty (1 + V_0/V_L) - x_i^0 V_0/V_L \end{aligned}$$

$$\begin{aligned} \frac{d(x^0)}{dt} &= \frac{A}{LV_0} \left(1 + \frac{V_0}{V_L} \right) [D] ((x^\infty) - (x^0)) \\ &= \beta [D] ((x^\infty) - (x^0)), \end{aligned}$$

Must solve this (coupled)
system of ODEs for the
change in the composition
in bulb 0 in time.

$$\beta \equiv \frac{A}{LV_0} \left(1 + \frac{V_0}{V_L} \right) \quad \text{Constant for a given geometry.}$$

Solution Strategy

$$\frac{d(x^0)}{dt} = \beta[D] ((x^\infty) - (x^0))$$

Solution Options:

- Solve this as a system of coupled ODEs.
- Make some assumptions to decouple the system.
- note: we have already made some assumptions to get the ODEs and the expression for (**J**).

Heat Transfer Analogy

From before: $\frac{\partial T}{\partial t} + \nabla \cdot \mathbf{v}T = \frac{k}{\rho c_p} \nabla^2 T,$

Steady state, $\mathbf{v}=0$: $\frac{d^2 T}{dz^2} = 0,$

Temperature solution: $T = \frac{T_L - T_0}{L} z + T_0,$

Heat flux: $q = -k \frac{dT}{dz} = -\frac{k}{L} (T_L - T_0).$

$$(x) = \frac{(x_L) - (x_0)}{L} z + (x_0)$$

$$(J) = -\frac{c_t}{L} [D] (x_L - x_0)$$

$$Le_{ij} = \frac{k}{\rho c_p D_{ij}}$$

If we know Le, ρ, k, c_p , we
can find D_{ij} . More later.