

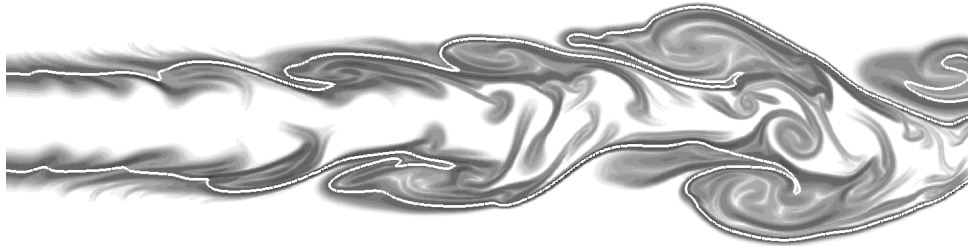
Mass Transfer in Turbulent Flow

ChEn 6603

References:

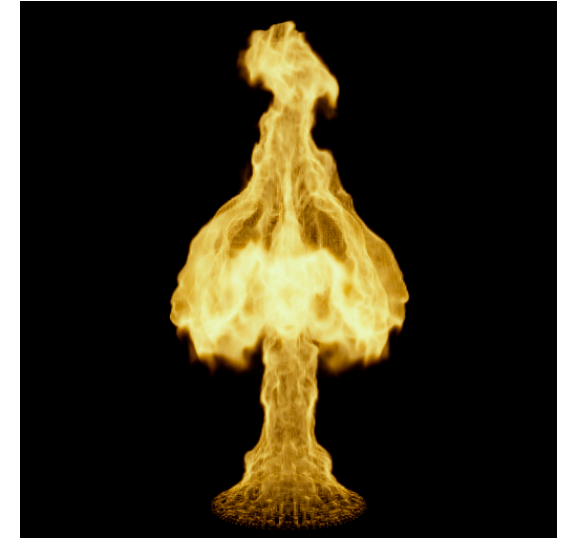
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- D. C. Wilcox. Turbulence Modeling for CFD. DCW Industries, La Caada CA, 2000.
- H. Tennekes and J. L. Lumley. A First Course in Turbulence. MIT Press, Cambridge, MA, 1972.
- R. O. Fox. Computational Models for Turbulent Reacting Flows. Cambridge University Press, 2003.

Mixing in reacting flow (DNS)

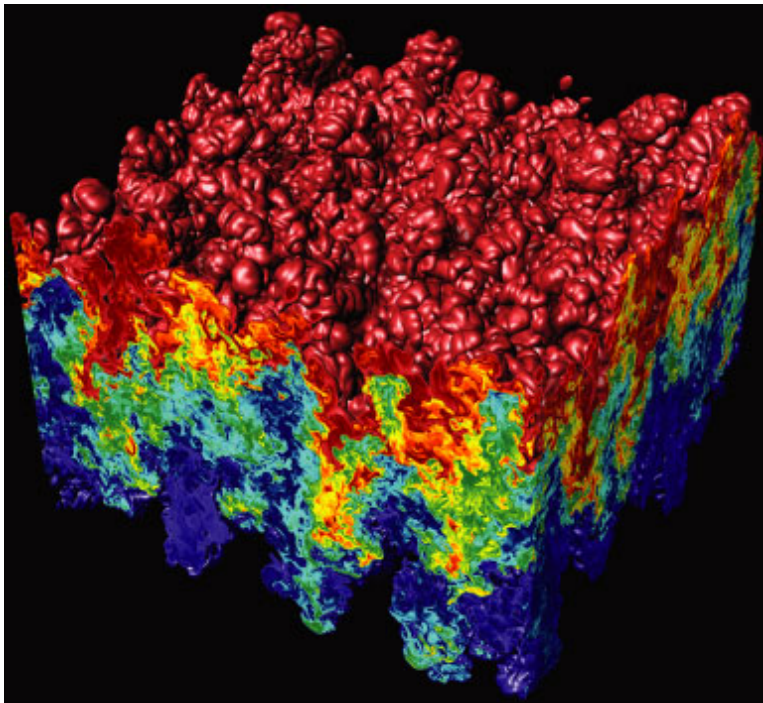


~ 6 cm

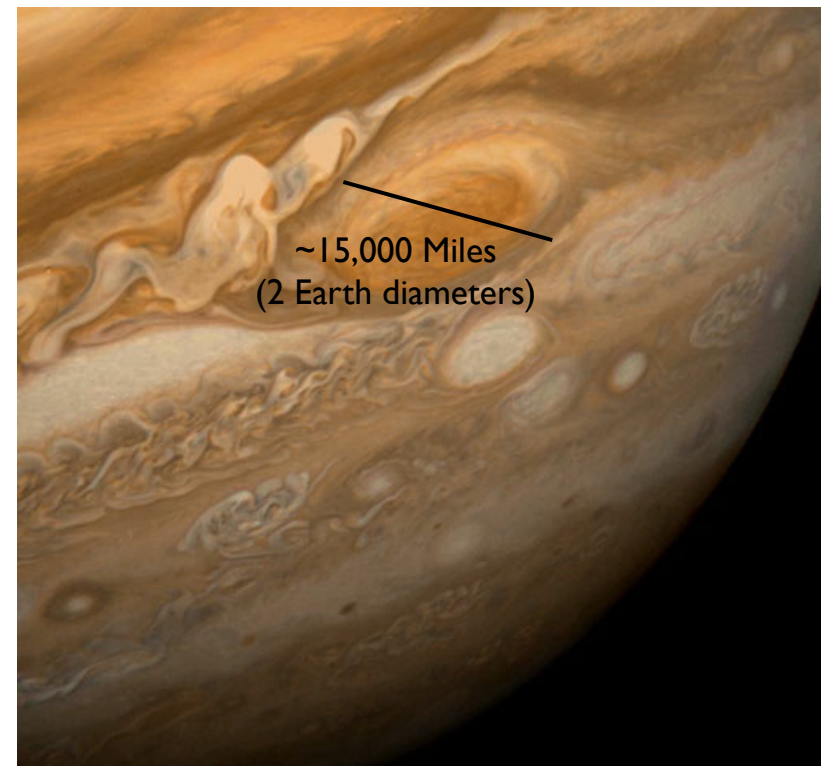
Methane pool fire



Rayleigh-Taylor instability (DNS calculation)



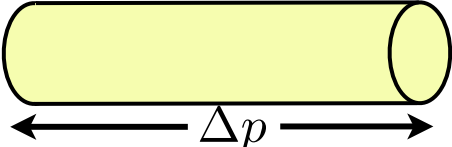
Photograph of Jupiter from Voyager



Origins of Turbulence


Energy balance perspective.

- Consider steady, isothermal, fully developed turbulent flow in a horizontal pipe
 - Increasing pressure drop does not increase flow rate proportionally. Why? Where is the energy going? How?
 - Work done by pressure forces balanced by work done by viscous forces
- Energy provided at “large” scales, dissipated at “small” scales.
 - Length scales reduce to meet demand of energy balance.
 - Smaller length scales \Rightarrow steeper gradients \Rightarrow more dissipation.



Kinetic energy equation:

$$\frac{\partial \rho k}{\partial t} + \nabla \cdot (\rho k \mathbf{v}) = -\mathbf{v} \cdot \nabla \cdot \boldsymbol{\tau} - \mathbf{v} \cdot \nabla p + \rho \sum_{i=1}^n \omega_i \mathbf{v} \cdot \mathbf{f}_i$$


What assumptions?

$$0 = \underbrace{\mathbf{v} \cdot \nabla p}_{\text{pressure work}} + \underbrace{\mathbf{v} \cdot \nabla \cdot \boldsymbol{\tau}}_{\text{viscous dissipation}}$$

Velocity Length Scales

L - largest length scale (m)
 η - smallest length scale (m)
 U - velocity at L -scale (m/s)

ν - kinematic viscosity (m^2/s) = μ/ρ
 ϵ - kinetic energy dissipation rate ($\text{m}^2/\text{s}^2 \cdot \text{s}^{-1}$)

Most kinetic energy is contained in “large” length scales (L).
 It is dissipated primarily at “smallest” (Kolmogorov) length scales (η) by molecular viscosity (ν).

Can we form a length scale from ϵ and ν ?

$$\eta \propto \left(\frac{\nu^3}{\epsilon} \right)^{1/4}$$

$$\epsilon \propto \frac{UU}{L/U} \quad \begin{array}{l} \text{kinetic energy} \\ \text{“integral” or “large” time scale} \end{array}$$

$$\eta \propto \left(\frac{\nu^3}{\epsilon} \right)^{1/4}$$

$$\propto L^{1/4} \left(\frac{\nu}{U} \right)^{3/4}$$

Note: ϵ doesn't depend on ν .
 ν just determines the smallest length scale in the flow.

$$\frac{L}{\eta} \propto \left(\frac{LU}{\nu} \right)^{3/4} = \text{Re}^{3/4}$$

Key result! Tells us how length-scales separate!

Scalar Length Scales

ℓ_B - smallest scalar length scale (Batchelor scale)

$$Sc \equiv \frac{\nu}{D}$$

$Sc > 1$

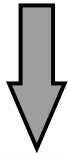
“mixing paint” - $\ell_B < \eta$ - scalar only feels straining from smallest velocity scales.
(mass diffuses slower than momentum)

$$\ell_B^2 \propto Dt$$

$$\ell_B \propto D^{1/2} \left(\frac{\nu}{\epsilon} \right)^{1/4}$$

$$\frac{\ell_B}{\eta} \propto D^{1/2} \left(\frac{\nu}{\epsilon} \right)^{1/4} \left(\frac{\nu^3}{\epsilon} \right)^{-1/4}$$

$$\propto \left(\frac{D}{\nu} \right)^{1/2} = Sc^{-1/2}$$



$$\frac{L}{\ell_B} = \frac{L}{\eta} \frac{\eta}{\ell_B} \propto Re^{3/4} Sc^{1/2}$$

Form a time scale from the “Kolmogorov” time scale (i.e. from ν and ϵ).

$Sc < 1$

$\ell_B > \eta$ - at ℓ_B , there are still velocity fluctuations, but the scalar field is uniform
(mass diffuses faster than momentum)

$$\ell_B \propto \left(\frac{D^3}{\epsilon} \right)^{1/4}$$

Relevant parameters are D, ϵ .
(ν only dominant near η).

$$\frac{\ell_B}{\eta} \propto \left(\frac{D}{\epsilon} \right)^{1/4} \left(\frac{\nu^3}{\epsilon} \right)^{-1/4}$$

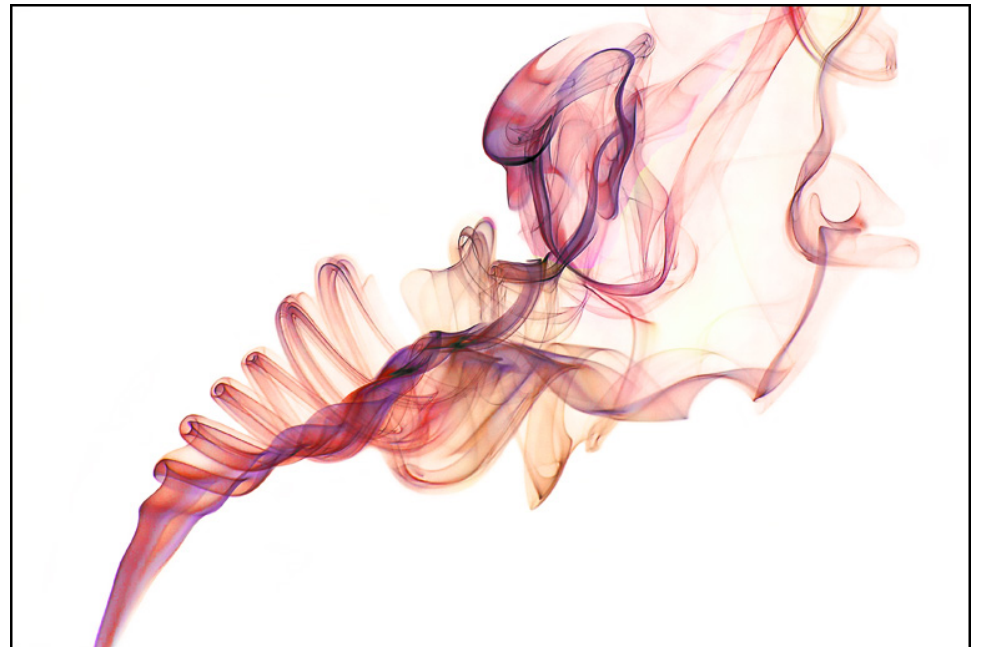
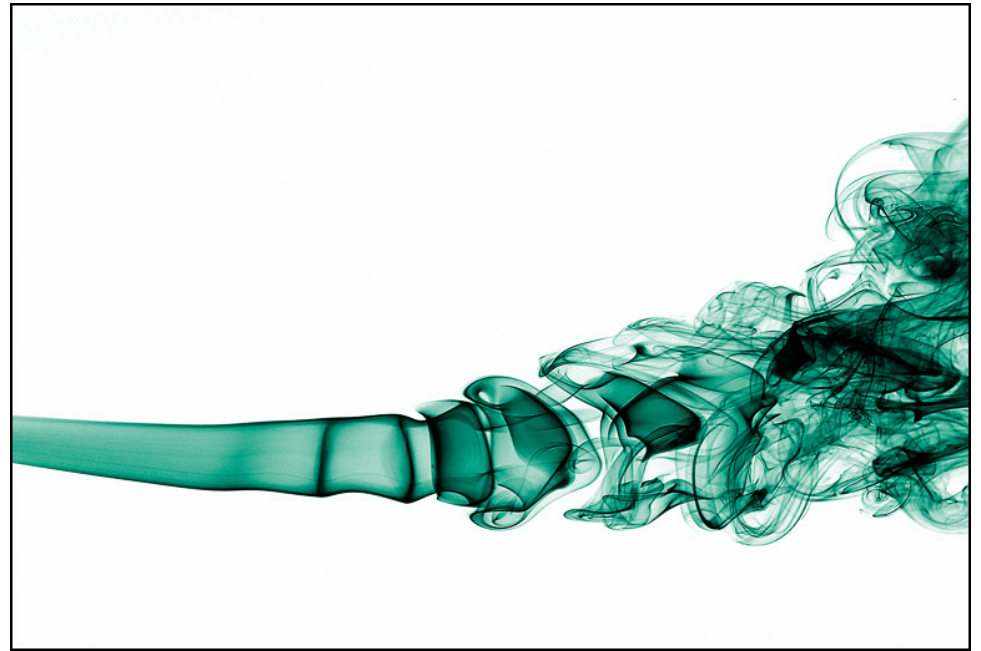
$$\propto \left(\frac{D}{\nu} \right)^{3/4} = Sc^{-3/4}$$



$$\frac{L}{\ell_B} = \frac{L}{\eta} \frac{\eta}{\ell_B} \propto Re^{3/4} Sc^{3/4}$$

Gases: $Sc \approx 1$, Liquids: $Sc \sim 10^3$.

$$Sc \rightarrow \infty$$



<http://sensitivelight.com/smoke2>

Solution Options

Increased Modeling

• Direct Numerical Simulation (DNS)

- Resolve all time/length scales by solving the governing equations directly.
- Restricted to small problems.
- Cost scales as Re^3 for turbulence alone! (Species with $Sc > 1$, and/or complex chemistry could further increase cost)
 - $(L/\eta \sim Re^{3/4}, 3D, \text{time})$

• Large Eddy Simulation (LES)

- Resolve “large” spatial & temporal scales
- Model “small” (unresolved) time/space scales

• Reynolds-Averaged Navier Stokes (RANS)

- Time-averaged.
- Describes only mean features of the flow.

• Model all effects of the flow field

- Useful only for some classes of problems (usually interfaces like walls)
- Commonly done in heat transfer & mass transfer (also for some problems involving aerodynamics)

Time/Ensemble Averaging (RANS)

Constant density, viscosity: $\nabla \cdot \mathbf{v} = 0$

$$\frac{\partial \mathbf{v}}{\partial t} = -\nabla \cdot (\mathbf{v} \otimes \mathbf{v}) - \frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{v}$$

$\langle \phi \rangle$ - ensemble average of ϕ .
 $\langle \nabla \phi \rangle = \nabla \langle \phi \rangle$

$$\bar{\phi} = \langle \phi \rangle$$

Continuity: $\langle \nabla \cdot \mathbf{v} \rangle = \langle 0 \rangle,$

$$\nabla \cdot \langle \mathbf{v} \rangle = 0,$$

$$\nabla \bar{\mathbf{v}} = 0$$

Momentum:

$$\left\langle \frac{\partial \mathbf{v}}{\partial t} \right\rangle = \left\langle -\nabla \cdot \mathbf{v} \mathbf{v} - \frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{v} \right\rangle,$$

$$\frac{\partial \langle \mathbf{v} \rangle}{\partial t} = -\nabla \cdot \langle \mathbf{v} \mathbf{v} \rangle - \frac{1}{\rho} \nabla \langle p \rangle + \nu \nabla^2 \langle \mathbf{v} \rangle,$$

$$\frac{\partial \bar{\mathbf{v}}}{\partial t} = -\nabla \cdot \bar{\mathbf{v} \mathbf{v}} - \frac{1}{\rho} \nabla \bar{p} + \nu \nabla^2 \bar{\mathbf{v}}$$

index (Einstein) notation:

$$\frac{\partial}{\partial x_j} \overline{v_i v_j} + \frac{1}{\rho} \frac{\partial \bar{p}}{\partial x_i} - \nu \frac{\partial}{\partial x_j} \frac{\partial \bar{v}_j}{\partial x_i} = 0$$

The Closure Problem

$$\phi' \equiv \phi - \bar{\phi} \quad \text{“Fluctuating” component}$$

$$\begin{aligned} \overline{v_i v_j} &= \overline{(\bar{v}_i + v'_i)(\bar{v}_j + v'_j)} \\ &= \overline{\bar{v}_i \bar{v}_j} + \overline{\bar{v}_i v'_j} + \overline{v'_i \bar{v}_j} + \overline{v'_i v'_j} \end{aligned}$$

$$\bar{\phi}' = 0 \quad \overline{\bar{\phi} \phi'} = 0 \quad \bar{\bar{\phi}} = \bar{\phi}$$

$$\overline{v_i v_j} = \bar{v}_i \bar{v}_j + \overline{v'_i v'_j}$$

$$\frac{\partial}{\partial x_j} (\bar{v}_i \bar{v}_j) + \frac{1}{\rho} \frac{\partial \bar{p}}{\partial x_i} - \nu \frac{\partial}{\partial x_j} \frac{\partial \bar{v}_j}{\partial x_i} + \boxed{\frac{\partial}{\partial x_j} (\overline{v'_i v'_j})} = 0$$

Model this term using a “gradient diffusion” model.

$$\frac{\partial}{\partial x_j} (\overline{v'_i v'_j}) \approx -\frac{\mu_t}{\rho} \frac{\partial}{\partial x_i} \frac{\partial}{\partial x_j} \bar{v}_j$$

$$\frac{\partial}{\partial x_j} (\bar{v}_i \bar{v}_j) + \frac{1}{\rho} \frac{\partial \bar{p}}{\partial x_i} - (\nu + \nu_t) \frac{\partial}{\partial x_j} \frac{\partial \bar{v}_j}{\partial x_i} = 0$$

For large Re, $\mu_t \gg \mu$ (molecular viscosity is negligible).

Time-Averaged Species Equations

constant properties & density...

$$\nabla \cdot \bar{\omega}_i \bar{\mathbf{v}} + \frac{1}{\rho} \nabla \cdot \bar{\mathbf{j}}_i = \boxed{\bar{s}_i} / \rho \quad \text{A very difficult problem...}$$

$$\nabla \cdot (\bar{\omega}_i \bar{\mathbf{v}}) + \frac{1}{\rho} \nabla \cdot \bar{\mathbf{j}}_i + \nabla \cdot (\overline{\omega'_i \mathbf{v}'}) = \bar{s}_i / \rho$$

$$\nabla \cdot (\bar{\omega}_i \bar{\mathbf{v}}) + \frac{1}{\rho} \nabla \cdot (\bar{\mathbf{j}}_i + \mathbf{j}_{i,\text{turb}}) = \bar{s}_i / \rho$$

MODEL for turbulent
species diffusive flux:

$$\mathbf{j}_{i,\text{turb}} = -\rho D_{\text{turb}}^{\circ} \nabla \bar{\omega}_i$$

$$Sc_{\text{turb}} = \frac{\nu_{\text{turb}}}{D_{\text{turb}}^{\circ}} = \frac{\mu_{\text{turb}}}{\rho D_{\text{turb}}^{\circ}}$$

- D_{turb}° - turbulent diffusivity (for mass flux relative to mass avg. velocity)
- μ_{turb} - eddy viscosity
- Typically, Sc_{turb} is specified.

@ Large Re, $\mathbf{j}_{i,\text{turb}} \gg \mathbf{j}_i$
(molecular diffusion is negligible)

$$\nabla \cdot (\bar{\omega}_i \bar{\mathbf{v}}) + \frac{1}{\rho} \nabla \cdot \mathbf{j}_{i,\text{turb}} = \bar{s}_i / \rho$$

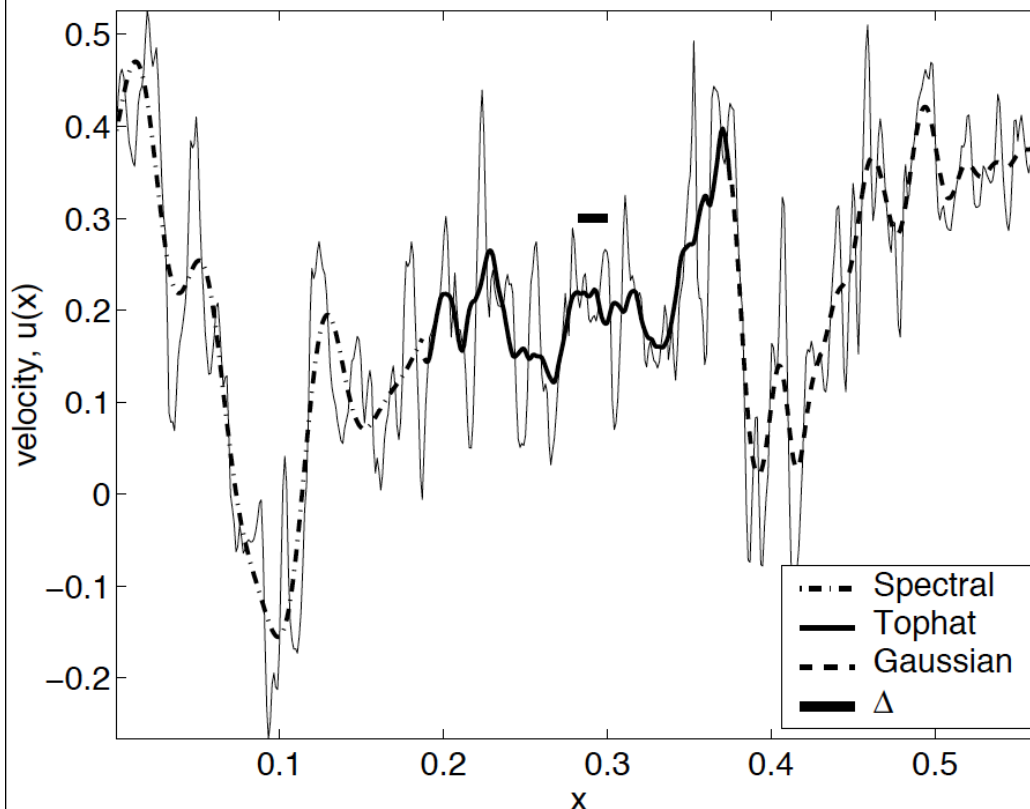
Multicomponent effects are irrelevant at sufficiently high Re.

Spatial Averaging (LES)

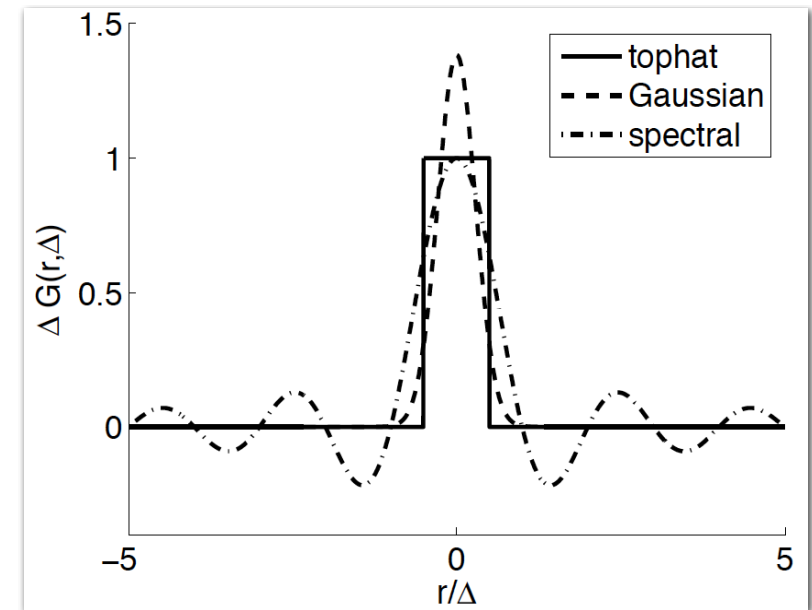
$$\bar{\phi} \equiv \int_{-\infty}^{\infty} \phi(\mathbf{x}) G(\mathbf{x}) d\mathbf{x}$$

$G(\mathbf{x})$ - filter kernel function

removes “high wavenumber” components of ϕ .



Courtesy R.J. McDermott



Courtesy R.J. McDermott

$$\begin{aligned} \bar{\phi} &\neq \bar{\phi} \\ \bar{\phi}' &\neq 0 \\ \overline{\phi\phi'} &\neq 0 \end{aligned}$$

- Filter governing equations. (similar procedure as for RANS, but a little more complicated).
- Write models for unclosed terms.
- Solve filtered equations (for filtered variables).
- Provides time-varying solutions at a “coarse” level.

Variable Density

$$\frac{\partial \rho \omega_i}{\partial t} = -\nabla \cdot \rho \omega_i \mathbf{v} - \nabla \cdot \mathbf{j}_i + s_i.$$

Favre-averaging (RANS)
Favre-filtering (LES)

$$\tilde{\phi} \equiv \frac{\overline{\rho \phi}}{\bar{\rho}} \longrightarrow \bar{\rho} \tilde{\phi} = \overline{\rho \phi}$$

$$\begin{aligned} \frac{\partial \bar{\rho} \tilde{\omega}_i}{\partial t} &= -\nabla \cdot \bar{\rho} \widetilde{\omega_i \mathbf{v}} - \nabla \cdot \bar{\mathbf{j}}_i + \bar{s}_i \\ &= -\nabla \cdot \bar{\rho} \tilde{\omega}_i \tilde{\mathbf{v}} - \nabla \cdot (\bar{\mathbf{j}}_i + \mathbf{j}_{i,\text{turb}}) + \bar{s}_i \end{aligned}$$

Leads to many additional complications,
most of which are typically ignored...

example:

$$\begin{aligned} \bar{\mathbf{j}}_i &= \sum_{k=1}^n \overline{\rho D_{ik}^o \nabla \omega_k} \\ &\stackrel{?}{\approx} \bar{\rho} \sum_{k=1}^n \bar{D}_{ik}^o \nabla \tilde{\omega}_k \end{aligned}$$

Δ = “filter width”

LES: if $\Delta \gg \ell_B, \Delta \gg \eta$ then $\mathbf{j}_{i,\text{turb}} \gg \bar{\mathbf{j}}_i$